

Control Systems UNIT 2

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- We can analyze the response of the control systems in both the time domain and the frequency domain.

If the output of control system for an input varies with respect to time, then it is called the time response of the control system. The time response consists of two parts.

- Transient response
- Steady state response

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Time
Response of
feedback
control
systems

Standard Test
Signals

Response of
First Order
System

Response of
Second Order
System

Case 1: $\delta = 0$
Undamping

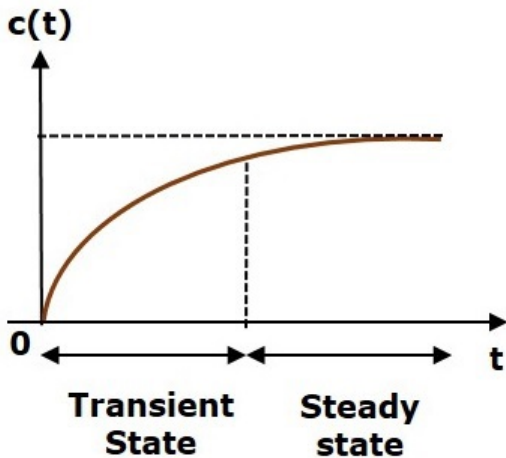
Case 2: $\delta = 1$
Critically damped
case

Case 3:
Underdamped case
($0 < \delta < 1$)

Case 4: Overdamped
case ($\delta > 1$)

Time response
specifications
and its
derivations

Steady State
Errors and
Error
constants



Here, both the transient and the steady states are indicated in the figure. The responses corresponding to these states are known as transient and steady state responses.

Mathematically, we can write the time response $c(t)$ as

$$c(t) = c_{tr}(t) + c_{ss}(t)$$

Where,

$c_{tr}(t)$ is the transient response

$c_{ss}(t)$ is the steady state response

- After applying input to the control system, output takes certain time to reach steady state. So, the output will be in transient state till it goes to a steady state. Therefore, the response of the control system during the transient state is known as transient response.
- The transient response will be zero for large values of t . Ideally, this value of t is infinity and practically, it is five times constant.
- Mathematically, we can write it as

$$\lim_{t \rightarrow \infty} c_{tr}(t) = 0$$

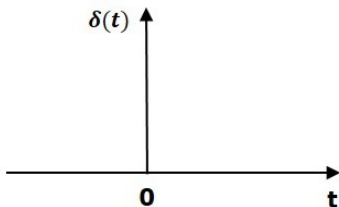
- The part of the time response that remains even after the transient response has zero value for large values of t is known as steady state response. This means, the transient response will be zero even during the steady state.
- Example:
Let us find the transient and steady state terms of the time response of the control system $c(t) = 10 + 5e^{-t}$
Here, the second term $5e^{-t}$ will be zero as t denotes infinity. So, this is the transient term. And the first term 10 remains even as t approaches infinity. So, this is the steady state term.

A unit impulse signal, $\delta(t)$ is defined as

$$\delta(t) = 0 \text{ for } t \neq 0$$

$$\text{and } \int_{0^-}^{0^+} \delta(t) dt = 1$$

The following figure shows unit impulse signal.



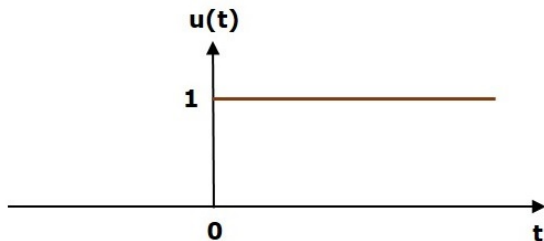
So, the unit impulse signal exists only at 't' is equal to zero. The area of this signal under small interval of time around 't' is equal to zero is one. The value of unit impulse signal is zero for all other values of 't'.

A unit step signal, $u(t)$ is defined as

$$u(t) = 1; t \geq 0$$

$$= 0; t < 0$$

Following figure shows unit step signal.



So, the unit step signal exists for all positive values of 't' including zero. And its value is one during this interval. The value of the unit step signal is zero for all negative values of 't'.

A unit ramp signal, $r(t)$ is defined as

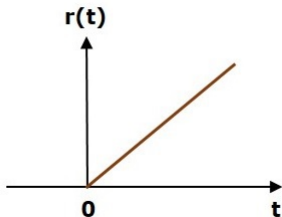
$$r(t) = t; t \geq 0$$

$$= 0; t < 0$$

We can write unit ramp signal, $r(t)$ in terms of unit step signal, $u(t)$ as

$$r(t) = tu(t)$$

Following figure shows unit ramp signal.



A unit parabolic signal, $p(t)$ is defined as,

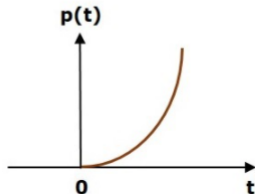
$$p(t) = \frac{t^2}{2}; t \geq 0$$

$$= 0; t < 0$$

We can write unit parabolic signal, $p(t)$ in terms of the unit step signal, $u(t)$ as,

$$p(t) = \frac{t^2}{2}u(t)$$

The following figure shows the unit parabolic signal.



- A linear time-invariant control system is stable if the output eventually comes back to its equilibrium state when the system is subjected to an initial condition.
- A linear time-invariant control system is critically stable if oscillations of the output continue forever.
- It is unstable if the output diverges without bound from its equilibrium state when the system is subjected to an initial condition.

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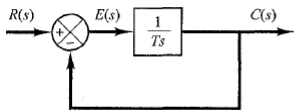
Case 3:
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($0 < \delta < 1$)

Case 4: Overdamped
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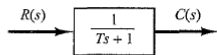
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Physically, RC circuit, thermal system etc.



(a)



(b)

We know that the transfer function of the closed loop control system has unity negative feedback as,

$$\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)}$$

Substitute, $G(s) = \frac{1}{sT}$ in the above equation.

$$\frac{C(s)}{R(s)} = \frac{\frac{1}{sT}}{1 + \frac{1}{sT}} = \frac{1}{sT + 1}$$

The power of s is one in the denominator term. Hence, the above transfer function is of the first order and the system is said to be the **first order system**.

We can re-write the above equation as

$$C(s) = \left(\frac{1}{sT + 1} \right) R(s)$$

Where,

- **C(s)** is the Laplace transform of the output signal $c(t)$,
- **R(s)** is the Laplace transform of the input signal $r(t)$, and
- **T** is the time constant.

Consider the **unit impulse signal** as an input to the first order system.

$$\text{So, } r(t) = \delta(t)$$

Apply Laplace transform on both the sides.

$$R(s) = 1$$

Consider the equation, $C(s) = \left(\frac{1}{sT+1}\right) R(s)$

Substitute, $R(s) = 1$ in the above equation.

$$C(s) = \left(\frac{1}{sT+1}\right) (1) = \frac{1}{sT+1}$$

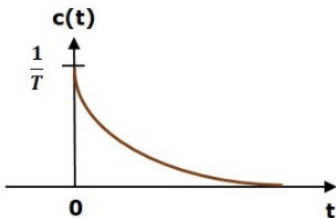
Rearrange the above equation in one of the standard forms of Laplace transforms.

$$C(s) = \frac{1}{T(s + \frac{1}{T})} \Rightarrow C(s) = \frac{1}{T} \left(\frac{1}{s + \frac{1}{T}} \right)$$

Apply inverse Laplace transform on both sides.

$$c(t) = \frac{1}{T} e^{-\frac{t}{T}} u(t)$$

The unit impulse response is shown in the following figure.



Consider the **unit step signal** as an input to first order system.

$$\text{So, } r(t) = u(t)$$

Apply Laplace transform on both the sides.

$$R(s) = \frac{1}{s}$$

Consider the equation, $C(s) = \left(\frac{1}{sT+1}\right) R(s)$

Substitute, $R(s) = \frac{1}{s}$ in the above equation.

$$C(s) = \left(\frac{1}{sT+1}\right) \left(\frac{1}{s}\right) = \frac{1}{s(sT+1)}$$

Do partial fractions of $C(s)$.

$$C(s) = \frac{1}{s(sT + 1)} = \frac{A}{s} + \frac{B}{sT + 1}$$

$$\Rightarrow \frac{1}{s(sT + 1)} = \frac{A(sT + 1) + Bs}{s(sT + 1)}$$

On both the sides, the denominator term is the same. So, they will get cancelled by each other. Hence, equate the numerator terms.

$$1 = A(sT + 1) + Bs$$

By equating the constant terms on both the sides, you will get $A = 1$.

Substitute, $A = 1$ and equate the coefficient of the s terms on both the sides.

$$0 = T + B \Rightarrow B = -T$$

Substitute, $A = 1$ and $B = -T$ in partial fraction expansion of $C(s)$.

$$C(s) = \frac{1}{s} - \frac{T}{sT + 1} = \frac{1}{s} - \frac{T}{T(s + \frac{1}{T})}$$

$$\Rightarrow C(s) = \frac{1}{s} - \frac{1}{s + \frac{1}{T}}$$

Apply inverse Laplace transform on both the sides.

$$c(t) = \left(1 - e^{-\left(\frac{t}{T}\right)}\right) u(t)$$

The **unit step response**, $c(t)$ has both the transient and the steady state terms.

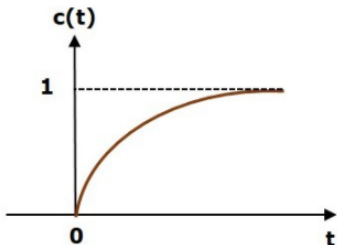
The transient term in the unit step response is -

$$c_{tr}(t) = -e^{-\left(\frac{t}{T}\right)} u(t)$$

The steady state term in the unit step response is -

$$c_{ss}(t) = u(t)$$

The following figure shows the unit step response.



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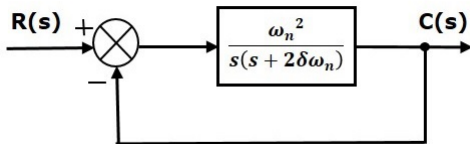
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We know that the transfer function of the closed loop control system having unity negative feedback as

$$\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)}$$

Substitute, $G(s) = \frac{\omega_n^2}{s(s+2\delta\omega_n)}$ in the above equation.

$$\frac{C(s)}{R(s)} = \frac{\left(\frac{\omega_n^2}{s(s+2\delta\omega_n)}\right)}{1 + \left(\frac{\omega_n^2}{s(s+2\delta\omega_n)}\right)} = \frac{\omega_n^2}{s^2 + 2\delta\omega_n s + \omega_n^2}$$

The power of 's' is two in the denominator term. Hence, the above transfer function is of the second order and the system is said to be the **second order system**.

The characteristic equation is -

$$s^2 + 2\delta\omega_n s + \omega_n^2 = 0$$

The roots of characteristic equation are -

$$s = \frac{-2\delta\omega_n \pm \sqrt{(2\delta\omega_n)^2 - 4\omega_n^2}}{2} = \frac{-2(\delta\omega_n \pm \omega_n\sqrt{\delta^2 - 1})}{2}$$

$$\Rightarrow s = -\delta\omega_n \pm \omega_n\sqrt{\delta^2 - 1}$$

- The two roots are imaginary when $\delta = 0$.
- The two roots are real and equal when $\delta = 1$.
- The two roots are real but not equal when $\delta > 1$.
- The two roots are complex conjugate when $0 < \delta < 1$.

We can write $C(s)$ equation as,

$$C(s) = \left(\frac{\omega_n^2}{s^2 + 2\delta\omega_n s + \omega_n^2} \right) R(s)$$

Where,

- $C(s)$ is the Laplace transform of the output signal, $c(t)$
- $R(s)$ is the Laplace transform of the input signal, $r(t)$
- ω_n is the natural frequency
- δ is the damping ratio.

Consider the unit step signal as an input to the second order system.

Laplace transform of the unit step signal is,

$$R(s) = \frac{1}{s}$$

We know the transfer function of the second order closed loop control system is,

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\delta\omega_n s + \omega_n^2}$$

Case 1: $\delta = 0$

Substitute, $\delta = 0$ in the transfer function.

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + \omega_n^2}$$

$$\Rightarrow C(s) = \left(\frac{\omega_n^2}{s^2 + \omega_n^2} \right) R(s)$$

Substitute, $R(s) = \frac{1}{s}$ in the above equation.

$$C(s) = \left(\frac{\omega_n^2}{s^2 + \omega_n^2} \right) \left(\frac{1}{s} \right) = \frac{\omega_n^2}{s(s^2 + \omega_n^2)}$$

Substitute, $R(s) = \frac{1}{s}$ in the above equation.

$$C(s) = \left(\frac{\omega_n^2}{s^2 + \omega_n^2} \right) \left(\frac{1}{s} \right) = \frac{\omega_n^2}{s(s^2 + \omega_n^2)}$$

Apply inverse Laplace transform on both the sides.

$$c(t) = (1 - \cos(\omega_n t)) u(t)$$

So, the unit step response of the second order system when $\delta = 0$ will be a continuous time signal with constant amplitude and frequency.

Case 2: $\delta = 1$

Substitute, $\delta = 1$ in the transfer function.

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\omega_n s + \omega_n^2}$$

$$\Rightarrow C(s) = \left(\frac{\omega_n^2}{(s + \omega_n)^2} \right) R(s)$$

Substitute, $R(s) = \frac{1}{s}$ in the above equation.

$$C(s) = \left(\frac{\omega_n^2}{(s + \omega_n)^2} \right) \left(\frac{1}{s} \right) = \frac{\omega_n^2}{s(s + \omega_n)^2}$$

Do partial fractions of $C(s)$.

$$C(s) = \frac{\omega_n^2}{s(s + \omega_n)^2} = \frac{A}{s} + \frac{B}{s + \omega_n} + \frac{C}{(s + \omega_n)^2}$$

After simplifying, you will get the values of A, B and C as $1, -1$ and $-\omega_n$ respectively.

Substitute these values in the above partial fraction expansion of $C(s)$.

$$C(s) = \frac{1}{s} - \frac{1}{s + \omega_n} - \frac{\omega_n}{(s + \omega_n)^2}$$

Apply inverse Laplace transform on both the sides.

$$c(t) = (1 - e^{-\omega_n t} - \omega_n t e^{-\omega_n t})u(t)$$

Case 3: $0 < \delta < 1$

We can modify the denominator term of the transfer function as follows -

$$\begin{aligned} s^2 + 2\delta\omega_n s + \omega_n^2 &= \{s^2 + 2(s)(\delta\omega_n) + (\delta\omega_n)^2\} + \omega_n^2 - (\delta\omega_n)^2 \\ &= (s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2) \end{aligned}$$

The transfer function becomes,

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)}$$

$$\Rightarrow C(s) = \left(\frac{\omega_n^2}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)} \right) R(s)$$

Substitute, $R(s) = \frac{1}{s}$ in the above equation.

$$C(s) = \left(\frac{\omega_n^2}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)} \right) \left(\frac{1}{s} \right) = \frac{\omega_n^2}{s((s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2))}$$

Do partial fractions of $C(s)$.

$$C(s) = \frac{\omega_n^2}{s((s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2))} = \frac{A}{s} + \frac{Bs + C}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)}$$

After simplifying, you will get the values of A, B and C as 1 , -1 and $-2\delta\omega_n$ respectively.

Substitute these values in the above partial fraction expansion of C(s).

$$C(s) = \frac{1}{s} - \frac{s + 2\delta\omega_n}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)}$$

$$C(s) = \frac{1}{s} - \frac{s + \delta\omega_n}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)} - \frac{\delta\omega_n}{(s + \delta\omega_n)^2 + \omega_n^2(1 - \delta^2)}$$

$$C(s) = \frac{1}{s} - \frac{(s + \delta\omega_n)}{(s + \delta\omega_n)^2 + (\omega_n\sqrt{1 - \delta^2})^2} - \frac{\delta}{\sqrt{1 - \delta^2}} \left(\frac{\omega_n\sqrt{1 - \delta^2}}{(s + \delta\omega_n)^2 + (\omega_n\sqrt{1 - \delta^2})^2} \right)$$

Substitute, $\omega_n\sqrt{1 - \delta^2}$ as ω_d in the above equation.

$$C(s) = \frac{1}{s} - \frac{(s + \delta\omega_n)}{(s + \delta\omega_n)^2 + \omega_d^2} - \frac{\delta}{\sqrt{1 - \delta^2}} \left(\frac{\omega_d}{(s + \delta\omega_n)^2 + \omega_d^2} \right)$$

Apply inverse Laplace transform on both the sides.

$$c(t) = \left(1 - e^{-\delta\omega_n t} \cos(\omega_d t) - \frac{\delta}{\sqrt{1-\delta^2}} e^{-\delta\omega_n t} \sin(\omega_d t) \right) u(t)$$

$$c(t) = \left(1 - \frac{e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} \left((\sqrt{1-\delta^2}) \cos(\omega_d t) + \delta \sin(\omega_d t) \right) \right) u(t)$$

If $\sqrt{1-\delta^2} = \sin(\theta)$, then 'δ' will be cos(θ). Substitute these values in the above equation.

$$c(t) = \left(1 - \frac{e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} (\sin(\theta) \cos(\omega_d t) + \cos(\theta) \sin(\omega_d t)) \right) u(t)$$

$$\Rightarrow c(t) = \left(1 - \left(\frac{e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t + \theta) \right) u(t)$$

So, the unit step response of the second order system is having damped oscillations (decreasing amplitude) when 'δ' lies between zero and one.

Case 4: $\delta > 1$

We can modify the denominator term of the transfer function as follows -

$$\begin{aligned} s^2 + 2\delta\omega_n s + \omega_n^2 &= \{s^2 + 2(s)(\delta\omega_n) + (\delta\omega_n)^2\} + \omega_n^2 - (\delta\omega_n)^2 \\ &= (s + \delta\omega_n)^2 - \omega_n^2 (\delta^2 - 1) \end{aligned}$$

The transfer function becomes,

$$\begin{aligned} \frac{C(s)}{R(s)} &= \frac{\omega_n^2}{(s + \delta\omega_n)^2 - \omega_n^2 (\delta^2 - 1)} \\ \Rightarrow C(s) &= \left(\frac{\omega_n^2}{(s + \delta\omega_n)^2 - \omega_n^2 (\delta^2 - 1)} \right) R(s) \end{aligned}$$

Substitute, $R(s) = \frac{1}{s}$ in the above equation.

$$C(s) = \left(\frac{\omega_n^2}{(s + \delta\omega_n)^2 - (\omega_n\sqrt{\delta^2 - 1})^2} \right) \left(\frac{1}{s} \right) = \frac{\omega_n^2}{s(s + \delta\omega_n + \omega_n\sqrt{\delta^2 - 1})(s + \delta\omega_n - \omega_n\sqrt{\delta^2 - 1})}$$

Do partial fractions of $C(s)$.

$$C(s) = \frac{\omega_n^2}{s(s + \delta\omega_n + \omega_n\sqrt{\delta^2 - 1})(s + \delta\omega_n - \omega_n\sqrt{\delta^2 - 1})}$$

$$= \frac{A}{s} + \frac{B}{s + \delta\omega_n + \omega_n\sqrt{\delta^2 - 1}} + \frac{C}{s + \delta\omega_n - \omega_n\sqrt{\delta^2 - 1}}$$

After simplifying, you will get the values of A, B and C as 1, $\frac{1}{2(\delta + \sqrt{\delta^2 - 1})(\sqrt{\delta^2 - 1})}$ and

$\frac{-1}{2(\delta - \sqrt{\delta^2 - 1})(\sqrt{\delta^2 - 1})}$ respectively. Substitute these values in above partial fraction expansion of

$$C(s) = \frac{1}{s} + \frac{1}{2(\delta + \sqrt{\delta^2 - 1})(\sqrt{\delta^2 - 1})} \left(\frac{1}{s + \delta\omega_n + \omega_n\sqrt{\delta^2 - 1}} \right) - \left(\frac{1}{2(\delta - \sqrt{\delta^2 - 1})(\sqrt{\delta^2 - 1})} \right) \left(\frac{1}{s + \delta\omega_n - \omega_n\sqrt{\delta^2 - 1}} \right)$$

Apply inverse Laplace transform on both the sides.

$$c(t) = \left(1 + \left(\frac{1}{2(\delta + \sqrt{\delta^2 - 1})(\sqrt{\delta^2 - 1})} \right) e^{-(\delta\omega_n + \omega_n\sqrt{\delta^2 - 1})t} - \left(\frac{1}{2(\delta - \sqrt{\delta^2 - 1})(\sqrt{\delta^2 - 1})} \right) e^{-(\delta\omega_n - \omega_n\sqrt{\delta^2 - 1})t} \right) u(t)$$

Since it is over damped, the unit step response of the second order system when $\delta > 1$ will never reach step input in the steady state.

- Damping is an influence within or upon an oscillatory system that has the effect of reducing or preventing its oscillation.
- In physical systems, damping is produced by processes that dissipate the energy stored in the oscillation.
- Examples include viscous drag in mechanical systems, resistance in electronic oscillators, and absorption and scattering of light in optical oscillators.
- The damping ratio is a dimensionless measure describing how oscillations in a system decay after a disturbance.

The effect of varying damping ratio on a second-order system.

Time Response of feedback control systems

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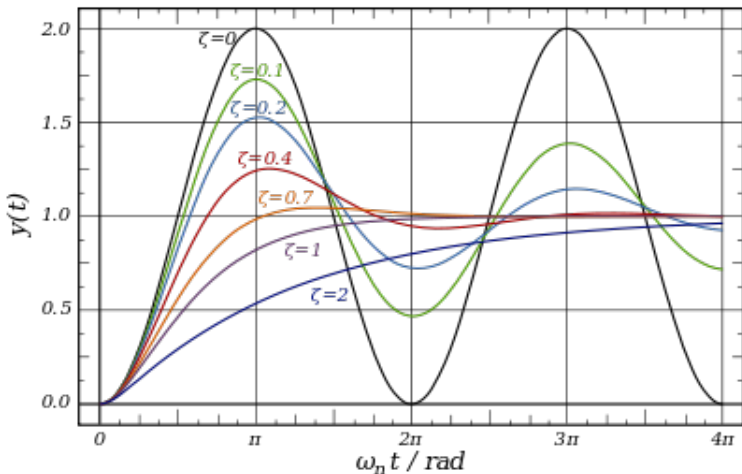
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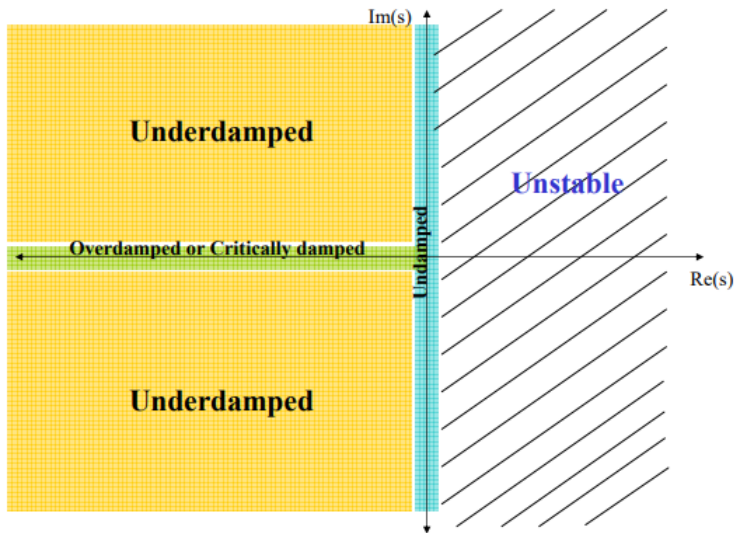
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Time response specifications and its derivations

Steady State Errors and Error constants





step response of the second order system for the underdamped case

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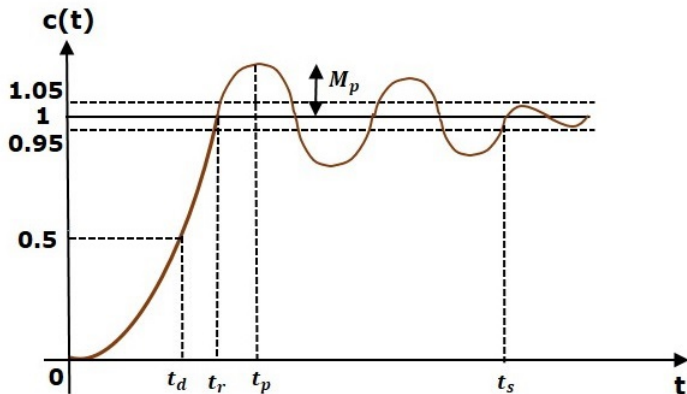
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The response up to the settling time is known as transient response and the response after the settling time is known as steady state response.

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- The time required for the response to reach 50% of the final value in the first time is called the delay time.

Consider the step response of the second order system for $t \geq 0$, when ' δ ' lies between zero and one.

$$c(t) = 1 - \left(\frac{e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t + \theta)$$

The final value of the step response is one.

Therefore, at $t = t_d$, the value of the step response will be 0.5. Substitute, these values in the above equation.

$$c(t_d) = 0.5 = 1 - \left(\frac{e^{-\delta\omega_n t_d}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t_d + \theta)$$

$$\Rightarrow \left(\frac{e^{-\delta\omega_n t_d}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t_d + \theta) = 0.5$$

By using linear approximation, you will get the **delay time t_d** as

$$t_d = \frac{1 + 0.7\delta}{\omega_n}$$

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Case 3:
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Case 4: Overdamped
case ($\delta > 1$)

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- The time required for response to rising from 10% to 90% of final value, for an overdamped system and 0 to 100% for an underdamped system is called the rise time of the system.

At $t = t_1 = 0$, $c(t) = 0$.

We know that the final value of the step response is one.

Therefore, at $t = t_2$, the value of step response is one. Substitute, these values in the following equation.

$$c(t) = 1 - \left(\frac{e^{-\delta\omega_n t}}{\sqrt{1 - \delta^2}} \right) \sin(\omega_d t + \theta)$$

$$c(t_2) = 1 = 1 - \left(\frac{e^{-\delta\omega_n t_2}}{\sqrt{1 - \delta^2}} \right) \sin(\omega_d t_2 + \theta)$$

$$\Rightarrow \left(\frac{e^{-\delta\omega_n t_2}}{\sqrt{1 - \delta^2}} \right) \sin(\omega_d t_2 + \theta) = 0$$

$$\Rightarrow \sin(\omega_d t_2 + \theta) = 0$$

$$\Rightarrow \omega_d t_2 + \theta = \pi$$

$$\Rightarrow t_2 = \frac{\pi - \theta}{\omega_d}$$

$$\Rightarrow t_2 = \frac{\pi - \theta}{\omega_d}$$

Substitute t_1 and t_2 values in the following equation of **rise time**,

$$t_r = t_2 - t_1$$

$$\therefore t_r = \frac{\pi - \theta}{\omega_d}$$

From above equation, we can conclude that the rise time t_r and the damped frequency ω_d are inversely proportional to each other.

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- It is the time required for the response to reach the peak value for the first time.

t_p . At $t = t_p$, the first derivative of the response is zero.

We know the step response of second order system for under-damped case is

$$c(t) = 1 - \left(\frac{e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t + \theta)$$

Differentiate $c(t)$ with respect to 't'.

$$\frac{dc(t)}{dt} = - \left(\frac{e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} \right) \omega_d \cos(\omega_d t + \theta) - \left(\frac{-\delta\omega_n e^{-\delta\omega_n t}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t + \theta)$$

Substitute, $t = t_p$ and $\frac{dc(t)}{dt} = 0$ in the above equation.

$$0 = - \left(\frac{e^{-\delta\omega_n t_p}}{\sqrt{1-\delta^2}} \right) [\omega_d \cos(\omega_d t_p + \theta) - \delta\omega_n \sin(\omega_d t_p + \theta)]$$

$$\Rightarrow \omega_n \sqrt{1 - \delta^2} \cos(\omega_d t_p + \theta) - \delta \omega_n \sin(\omega_d t_p + \theta) = 0$$

$$\Rightarrow \sqrt{1 - \delta^2} \cos(\omega_d t_p + \theta) - \delta \sin(\omega_d t_p + \theta) = 0$$

$$\Rightarrow \sin(\theta) \cos(\omega_d t_p + \theta) - \cos(\theta) \sin(\omega_d t_p + \theta) = 0$$

$$\Rightarrow \sin(\theta - \omega_d t_p - \theta) = 0$$

$$\Rightarrow \sin(-\omega_d t_p) = 0 \Rightarrow -\sin(\omega_d t_p) = 0 \Rightarrow \sin(\omega_d t_p) = 0$$

$$\Rightarrow \omega_d t_p = \pi$$

$$\Rightarrow t_p = \frac{\pi}{\omega_d}$$

From the above equation, we can conclude that the peak time t_p and the damped frequency

ω_d are inversely proportional to each other.

- The difference between the peak of 1st time and steady output is called the peak overshoot. It is also called the maximum overshoot.

Mathematically, we can write it as

$$M_p = c(t_p) - c(\infty)$$

Where,

$c(t_p)$ is the peak value of the response.

$c(\infty)$ is the final (steady state) value of the response.

At $t = t_p$, the response $c(t)$ is -

$$c(t_p) = 1 - \left(\frac{e^{-\delta\omega_n t_p}}{\sqrt{1-\delta^2}} \right) \sin(\omega_d t_p + \theta)$$

Substitute, $t_p = \frac{\pi}{\omega_d}$ in the right hand side of the above equation.

$$c(t_p) = 1 - \left(\frac{e^{-\delta\omega_n \left(\frac{\pi}{\omega_d}\right)}}{\sqrt{1-\delta^2}} \right) \sin\left(\omega_d \left(\frac{\pi}{\omega_d}\right) + \theta\right)$$

$$\Rightarrow c(t_p) = 1 - \left(\frac{e^{-\left(\frac{\delta\pi}{\sqrt{1-\delta^2}}\right)}}{\sqrt{1-\delta^2}} \right) (-\sin(\theta))$$

We know that

$$\sin(\theta) = \sqrt{1 - \delta^2}$$

So, we will get $c(t_p)$ as

$$c(t_p) = 1 + e^{-\left(\frac{\delta \pi}{\sqrt{1 - \delta^2}}\right)}$$

Substitute the values of $c(t_p)$ and $c(\infty)$ in the peak overshoot equation.

$$M_p = 1 + e^{-\left(\frac{\delta \pi}{\sqrt{1 - \delta^2}}\right)} - 1$$

$$\Rightarrow M_p = e^{-\left(\frac{\delta \pi}{\sqrt{1 - \delta^2}}\right)}$$

Percentage of peak overshoot $\%M_p$ can be calculated by using this formula.

$$\%M_p = \frac{M_p}{c(\infty)} \times 100\%$$

By substituting the values of M_p and $c(\infty)$ in above formula, we will get the Percentage of the peak overshoot $\%M_p$ as

$$\%M_p = \left(e^{-\left(\frac{\delta \pi}{\sqrt{1-\delta^2}}\right)} \right) \times 100\%$$

From the above equation, we can conclude that the percentage of peak overshoot $\%M_p$ will decrease if the damping ratio δ increases.

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- The time that is required for the response to reach and stay within the specified range (2% to 5%) of its final value is called the settling time.

The settling time for 5% tolerance band is -

$$t_s = \frac{3}{\delta\omega_n} = 3\tau$$

The settling time for 2% tolerance band is -

$$t_s = \frac{4}{\delta\omega_n} = 4\tau$$

Where, τ is the time constant and is equal to $\frac{1}{\delta\omega_n}$.

- Both the settling time t_s and the time constant τ are inversely proportional to the damping ratio δ .
 - Both the settling time t_s and the time constant τ are independent of the system gain.
- That means even the system gain changes, the settling time t_s and time constant τ will never change.

- Find the time domain specifications of a control system having the closed loop transfer function $\frac{4}{s^2+2s+4}$ when the unit step signal is applied as an input to this control system.

We know that the standard form of the transfer function of the second order closed loop control system as

$$\frac{\omega_n^2}{s^2 + 2\delta\omega_n s + \omega_n^2}$$

By equating these two transfer functions, we will get the un-damped natural frequency ω_n as 2 rad/sec and the damping ratio δ as 0.5.

We know the formula for damped frequency ω_d as

$$\omega_d = \omega_n \sqrt{1 - \delta^2}$$

Substitute, ω_n and δ values in the above formula.

$$\Rightarrow \omega_d = 2\sqrt{1 - (0.5)^2}$$

$$\Rightarrow \omega_d = 1.732 \text{ rad/sec}$$

Substitute, δ value in following relation

$$\theta = \cos^{-1} \delta$$

$$\Rightarrow \theta = \cos^{-1}(0.5) = \frac{\pi}{3} \text{ rad}$$

Time domain specification	Formula	Substitution of values in Formula	Final value
Delay time	$t_d = \frac{1+0.7\delta}{\omega_n}$	$t_d = \frac{1+0.7(0.5)}{2}$	$t_d = 0.675$ sec
Rise time	$t_r = \frac{\pi - \theta}{\omega_d}$	$t_r = \frac{\pi - (\frac{\pi}{3})}{1.732}$	$t_r = 1.207$ sec
Peak time	$t_p = \frac{\pi}{\omega_d}$	$t_p = \frac{\pi}{1.732}$	$t_p = 1.813$ sec
% Peak overshoot	$\%M_p = \left(e^{-\left(\frac{\delta\pi}{\sqrt{1-\delta^2}}\right)} \right) \times 100\%$	$\%M_p = \left(e^{-\left(\frac{0.5\pi}{\sqrt{1-(0.5)^2}}\right)} \right) \times 100\%$	$\%M_p = 16.32\%$
Settling time for 2% tolerance band	$t_s = \frac{4}{\delta\omega_n}$	$t_s = \frac{4}{(0.5)(2)}$	$t_s = 4$ sec

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Case 1: $\delta = 0$
Undamping

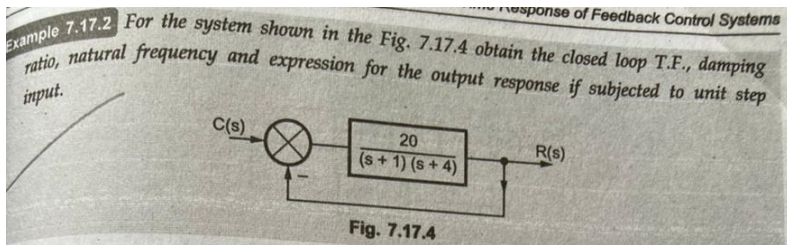
Case 2: $\delta = 1$
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case

Case 3:
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$$\text{Solution : } \frac{C(s)}{R(s)} = \frac{\frac{20}{(s+1)(s+4)}}{1 + \frac{20}{(s+1)(s+4)}} = \frac{20}{s^2 + 5s + 24}$$

Key Point Now though T.F. is not in standard form, denominator always reflect $2\xi\omega_n$ and ω_n^2 from middle term and the last term respectively.

\therefore Comparing, $s^2 + 5s + 24$ with $s^2 + 2\xi\omega_n s + \omega_n^2$

$$\therefore \omega_n^2 = 24 \quad \therefore \omega_n = 4.8989 \text{ rad/sec.}$$

$$2\xi\omega_n = 5 \quad \therefore \xi = 0.51031$$

$$\omega_d = \omega_n \sqrt{1 - \xi^2} = 4.2129 \text{ rad/sec.}$$

Now, for $c(t)$ we can use standard expression for $\frac{C(s)}{R(s)}$ in standard form. So writing

$$\frac{C(s)}{R(s)} = \frac{20}{24} \cdot \left\{ \frac{24}{s^2 + 5s + 24} \right\}$$

For the bracket term use standard expression, and then $c(t)$ can be obtained by multiplying this expression by constant $\frac{20}{24}$.

$$\therefore c(t) = \frac{20}{24} \left[1 - \frac{e^{-\xi \omega_n t}}{\sqrt{1-\xi^2}} \sin(\omega_d t + \theta) \right]$$

$$\theta = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi} \text{ radians} = 1.03 \text{ radians}$$

$$\therefore c(t) = \frac{20}{24} \left[1 - 1.1628 e^{-2.5t} \sin(4.2129 t + 1.03) \right]$$

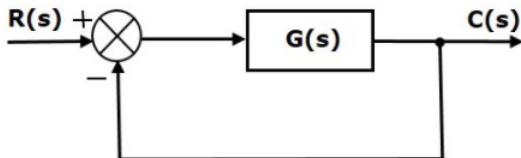
The deviation of the output of control system from desired response during steady state is known as **steady state error**. It is represented as e_{ss} . We can find steady state error using the final value theorem as follows.

$$e_{ss} = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} sE(s)$$

Where,

$E(s)$ is the Laplace transform of the error signal, $e(t)$

Consider the following block diagram of closed loop control system, which is having unity negative feedback.



Where,

- $R(s)$ is the Laplace transform of the reference input signal $r(t)$
- $C(s)$ is the Laplace transform of the output signal $c(t)$

We know the transfer function of the unity negative feedback closed loop control system as

$$\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)}$$

$$\Rightarrow C(s) = \frac{R(s)G(s)}{1 + G(s)}$$

The output of the summing point is -

$$E(s) = R(s) - C(s)$$

Substitute $C(s)$ value in the above equation.

$$E(s) = R(s) - \frac{R(s)G(s)}{1 + G(s)}$$

Substitute $C(s)$ value in the above equation.

$$E(s) = R(s) - \frac{R(s)G(s)}{1 + G(s)}$$

$$\Rightarrow E(s) = \frac{R(s) + R(s)G(s) - R(s)G(s)}{1 + G(s)}$$

$$\Rightarrow E(s) = \frac{R(s)}{1 + G(s)}$$

Substitute $E(s)$ value in the steady state error formula

$$e_{ss} = \lim_{s \rightarrow 0} \frac{sR(s)}{1 + G(s)}$$

Steady State Errors and the error constants for standard input signals

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Input signal	Steady state error e_{ss}	Error constant
unit step signal	$\frac{1}{1+k_p}$	$K_p = \lim_{s \rightarrow 0} G(s)$
unit ramp signal	$\frac{1}{K_v}$	$K_v = \lim_{s \rightarrow 0} sG(s)$
unit parabolic signal	$\frac{1}{K_a}$	$K_a = \lim_{s \rightarrow 0} s^2G(s)$

Where, K_p , K_v and K_a are position error constant, velocity error constant and acceleration error constant respectively.

Example Steady State Errors for Unity Feedback Systems

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Example 7.8.1 An unity feedback system has $G(s) = \frac{20(1+s)}{s^2(2+s)(4+s)}$, calculate its steady state error co-efficients and error when the applied input $r(t) = 40 + 2t + 5t^2$.

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Solution :
$$G(s)H(s) = \frac{20(1+s)}{s^2(2+s)(4+s)} = \frac{20(1+s)}{s^2 \times 2 \left(1 + \frac{s}{2}\right) \times 4 \left(1 + \frac{s}{4}\right)}$$

$$\therefore G(s)H(s) = \frac{2.5(1+s)}{s^2(1+0.5s)(1+0.25s)} \quad \dots \text{St}$$

Thus $j = 2$ hence it is Type 2 system

$$K_p = \lim_{s \rightarrow 0} G(s)H(s) = \lim_{s \rightarrow 0} \frac{2.5(1+s)}{s^2(1+0.5s)(1+0.25s)} = \infty$$

$$K_v = \lim_{s \rightarrow 0} sG(s)H(s) = \lim_{s \rightarrow 0} \frac{s \times 2.5(1+s)}{s^2(1+0.5s)(1+0.25s)} = \infty$$

Example Steady State Errors for Unity Feedback Systems

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$$K_a = \lim_{s \rightarrow 0} s^2 G(s)H(s) = \lim_{s \rightarrow 0} \frac{s^2 \times 2.5(1+s)}{s^2(1+0.5s)(1+0.25s)} = 2.5$$

$$r(t) = 40 + 2t + 5t^2 = 40 + 2t + \frac{10}{2}t^2 = A_1 + A_2 t + \frac{A_3}{2}t^2$$

Hence $A_1 = 40$ step, $A_2 = 2$ ramp, $A_3 = 10$ parabolic

$$\therefore e_{ss} = e_{ss1} + e_{ss2} + e_{ss3} = \frac{A_1}{1+K_p} + \frac{A_2}{K_v} + \frac{A_3}{K_a}$$

$$\therefore e_{ss} = \frac{40}{1+\infty} + \frac{2}{\infty} + \frac{10}{2.5} = 0 + 0 + 4 = 4$$

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The End